Liquid Phase Crystallized Silicon – A Holistic Absorber Quality Assessment

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Liquid Phase Crystallized -Silicon (LPC-Si), the basis for multi-crystalline thin-film solar cells with absorber thicknesses around 15 µm, is subject to rapid quality improvements. Recently, power conversion efficiencies surpassed 13%. With open circuit voltages above 650 mV and grain sizes of up to cm in length, LPC-Si morphology and electronic quality has reached mc-Si wafer quality. In this paper, we report on the current status of absorber attributes in LPC-Si cells. To this end, an absorber doping series and an absorber thickness variation are evaluated. It is observed that for state-of-the-art cells, thicknesses over 15 µm are not beneficial due to limited diffusion lengths. Lower absorber doping concentrations tend to yield longer intra-grain diffusion lengths ($L_{diff}$) and better passivated grain boundaries, which may be due to lower impurity precipitation. The longer $L_{diff}$ leads to higher short circuit current densities which over-compensate a decrease in open circuit voltage and fill factor with regards to efficiency. Both front and rear surfaces are sufficiently passivated and at the current status the bulk lifetime has most potential for improvement.

I. INTRODUCTION

Many approaches are being pursued to bring down material consumption of Si solar cells using the wafering process by alternative fabrication techniques. These alternatives include classical thin-film technologies like amorphous (a-Si) or microcrystalline (µ-c-Si) Si [1–3], top-down approaches like epitaxial lift-off techniques [4,5] or the liquid phase crystallization (LPC) technology [6]. All of them offer the potential to save material cost while having the advantage to rely on a vast existing knowledge on (crystalline) Si photovoltaics.

LPC of Si absorbers is a zone-melting procedure using a line-shaped energy source to convert an initially amorphous/nano-crystalline precursor to multi-crystalline material directly on a supporting glass with multi-functional thin (200 nm) intermediate layers [6]. In contrast to a-Si/µc-Si absorbers [7] LPC-Si absorbers can be up to 40 µm thick and show grain sizes comparable to multi-crystalline(mc)-Si wafers [8,9]. The technology represents thus a hybrid between wafers and classical bottom-up thin-film technologies. Contrary to that, the elaborate top-down epitaxial lift-off technique uses a high quality mono-crystalline and reusable parent wafer from which absorbers are lifted off and bonded to a substrate [4,5]. Efficiencies of up to 20.6% were presented on 35 µm Si [10]. With the a-Si/µc-Si tandem technology, recently, a 14% cell was achieved [3]. Present efficiencies on LPC-Si are 13.2% on below 15 µm thick absorbers using an interdigitated back contact (IBC) system and up to 15.9% on full-emitter test structures [11]. LPC-Si has shown a steep learning curve and progress in recent years, amongst other, thanks to a continuous improvement of the quality of the interface between Si and the supporting glass by an intermediate layer (IL) stack [12,13] and hydrogen plasma passivation techniques [14]. To push performance even further, a thorough material assessment is necessary to find possible levers for improvement. However, many standard wafer characterization methods do not work due to poor signal/noise ratio (quasi steady state photo conduction, QSSPC) or challenging to evaluate because of substrate effects (photoluminescence, PL). Although it was shown that QSSPC can be measured with under certain circumstances with an altered setup[15], symmetrical lifetime samples can inherently not be processed, because an identical surface treatment as for the buried and inaccessible LPC-Si/supporting glass side cannot be repeated on the other side. Hence, in this publication, we obtain material parameters from illuminated $J$-$V$-curves of finished devices and compare them to simulations. The studied devices are bifacial so comparing the two illumination configurations (i) through the glass (superstrate) and (ii) from Si side (substrate) conclusions about the glass/LPC-Si interface quality can be drawn. Furthermore, the change in absorber quality of LPC-Si absorbers with varying phosphorous doping concentration is partly quantified using light beam induced current measurements and $J$-$V$ measurements.

II. EXPERIMENTAL

LPC-Si absorbers were fabricated according to the steps in [11]. For the doping series, 15 µm and for the thickness variation 14 and 33 µm of nominally intrinsic Si were
deposited on 1.1 mm Corning Eagle XG glass using high rate electron beam evaporation. Prior to Si deposition a multi-functional intermediate layer (IL) comprised of SiO$_x$/SiN$_x$/SiO$_x$ was deposited as described elsewhere [12,13,16]. Amongst others, this IL is crucial for final device performance, since it is the only option to control the passivation and stop impurity diffusion at the glass/LPC-Si interface because later this interface is buried and inaccessible. Subsequent to absorber precursor deposition, a so-called doping layer comprised of a-Si:H(n) was deposited by PECVD to introduce phosphorous (P) dopants. Different final doping concentrations were achieved by varying the phosphine gas flow during deposition. The actual liquid phase crystallization procedure was performed using a line-shaped laser at a wavelength of 808 nm in vacuum [12]. The absorber is molten entirely, allowing the dopants in the doping layer to disperse homogeneously throughout the absorber. Final doping densities between 2.0·10$^{16}$ and 7.0·10$^{17}$ /cm$^3$ were reached this way. The doping densities were determined by sheet resistance measurements according to

$$N_D = \left(\frac{eR_{\text{sheet}} \mu_n d_0}{\bar{R}_{\text{sheet}}}ight)^{-1}$$  \hspace{1cm} (1)

$\bar{R}_{\text{sheet}}$ being the averaged sheet resistance of measurements on the entire substrate and the elementary charge $e$, initial absorber thickness $d_0$ and majority carrier (electron) mobility $\mu_n$.

The latter was assumed to be 80 % of the mobilities of the Masetti model [17] for mono-crystalline Si to account for the poly-crystalline structure. This is in accordance with earlier findings [8,9,14]. An error for the resulting $N_D$ was calculated from the standard deviation of all $R_{\text{sheet}}$ measurements. To augment absorber quality a hydrogen plasma treatment [12,14] was performed prior to contact system processing. Finally, interdigitated back contact (IBC) cells using silicon heterojunctions (SHJ) were fabricated on the absorbers for the doping series (Fig. 1 (a,c)). Bifacial circular cell test structures (quasi cells, Fig. 1(b,d)) having the lowest doping concentration of the doping series were processed on the absorbers for the thickness variation. Both will be introduced in detail in the following.

A. Interdigitated Back Contact Cells

A cross section of an IBC-SHJ unit cell (pitch) is shown schematically in Fig. 1(a) and a photograph of the back (metal) side of a whole cell is depicted in Fig. 1(c). The red dotted line indicates the length of the cross section in (a). The red full rectangle represents the area of the cell (emitter busbar is also counted as cell area). The whole fabrication process in elaborate detail can be found in [11]. In total 44 cells were processed on 4 substrates of doping densities of 2.0·10$^{16}$, 1.4·10$^{17}$, 1.7·10$^{17}$ and 7.0·10$^{17}$ /cm$^3$. The contact system was co-processed for all cells in the same run and all cells received identical wet chemistry treatment.

B. Quasi Cell Test Structures

A schematic cross section of a quasi cell test structure and a top-view photograph can be seen in Fig. 1(b) and (d), respectively. The sun-pictographs indicate that operation in substrate (front-emitter) and superstrate (rear-emitter) configuration is possible. The cell diameter is 8 mm corresponding to an emitter area of ~0.5 cm$^2$. The absorber contact is not passivated and lies outside the defined cell area (cp. red circle in (d)). On one hand the cell has an inherently low fill factor (FF) due to a high base series resistance. On the other hand, it is comparably simple to fabricate, fully bifacial and useful for screening short circuit current density ($J_{SC}$) and open circuit voltage ($V_{OC}$). The surfaces of the $N_D=2·10^{16}$/cm$^2$ absorbers are first cleaned and an a-Si:H(i/p) emitter is formed using low-temperature PECVD. Subsequently, 80 nm ITO is RF-sputtered from a ceramic target. The cell area is defined by an adhesive masking tape with circular shape of 4 mm radius made of Kapton® polyimide film with silicone adhesive by Max Steier GmbH & Co. KG. Subsequent to mask-taping the ITO surface, the samples were etched for 10 s in 20 % HCl to

![Figure 1](https://example.com/figure1.png)

*Figure 1: (a) Schematic cross section of one pitch length of an IBC-SHJ cell on LPC-Si on glass. (b) Schematic cross section of a whole quasi cell test structure. (c) Photograph of top-view of an IBC-SHJ (back side). The cell area is indicated by the red full line. The location of the cross section in (a) is indicated by the red dotted line. (d) Top-view of quasi cell test structures in substrate configuration. Red circle indicates cell area, red dotted line the place of the cross section in (b).*
remove the ITO surrounding the Kapton®dots. In the second etch step of 15-20 s, in a mixture of nitric, phosphorous, and hydrofluoric acid, possible remains of the ITO are removed and the a-Si:H(i/p) emitter is dissolved. After the HF-dip, the samples were thermally coated with 30 nm Ti and 1000 nm Al. The Kapton®dots are temperature resistant up to 270°C and not affected during all the acidic treatments. Finally, the dots were removed exposing the finished quasi cell test structures depicted in Figure 1(d). Since all the etching solutions used creep also (on a µm scale) underneath the Kapton®dots an isolation gap is inherently formed during the process between the ITO contact which serves as p-type contact, and the Ti/Al absorber (n-type) contact.

C. Methods

Illuminated J-V curves were recorded with a dual source solar simulator by Wacom having AAA characteristics [18].

LBIC measurements were conducted using a self-built setup at the University of Ljubljana with a laser of 638 nm wavelength, a spot size below 10 µm and an x,y,z stage with minimum step width of 1 µm [19].

Simulations were performed using ASPIN3, a numerical 2D solar cell simulation software, developed at the University of Ljubljana [20].

III. Results

A. Doping Series

The main parameters obtained from the recorded illuminated J-V-curves of all the 44 fabricated cells are shown in Figure 2 except for 3 outliers. The fluctuation in performance leading to the standard deviation of measurements shown as error bars can be attributed to the inhomogeneous mc-Si-like morphology of LPC-Si. We observe a strong decrease of $J_{SC}$ with higher doping (red) and a slight increase of $V_{OC}$ (blue) that seems to decrease again for $N_D = 7.0\cdot10^{17}/cm^3$. The $FF$ tends to increase with doping (orange), while overall conversion efficiency drops steadily (green), following the trend of $J_{SC}$. Please note that to reach current densities above 30 mA/cm² as in [21,22] a light trapping foil is usually additionally placed on the front glass which has been omitted here. Black circles and triangles are calculated $V_{OC}$ values that will be explained in the discussion section.

Light beam induced current (LBIC) measurements of the best cells with $N_D = 2.0\cdot10^{16}$, $1.7\cdot10^{17}$ and $7.0\cdot10^{17}/cm^3$ were recorded to investigate grain boundary (GB) behavior and evaluate diffusion lengths using a method presented in [23]. The method uses LBIC line-scans to measure the collection signal drop at the absorber contact, where no minority carriers are collected. A measure for this signal drop is the effective diffusion length $L_{diff}$ (taking bulk and interface effects into account) which is obtained by a double exponential fit of the line-scans [23]. The cells on the substrate containing $N_D = 1.4\cdot10^{17}/cm^3$ were omitted, since it is very close to the one of $1.7\cdot10^{17}/cm^3$. The complete LBIC 2D collection maps are shown in Figure 3 (a-c). The images were all scaled from 0 to the median of all pixel values. All areas with values above the median appear white. The absorber contacts appear black, since the minority charge carriers generated in this region have to travel laterally to the minority contacts (“electrical shading”). Other areas of reduced collection are due to multi-crystalline nature of LPC-Si (GBs and dislocations). It can be seen that the GBs of the cell with $N_D = 7.0\cdot10^{17}/cm^3$ are substantially better visible due to a higher signal drop caused by higher recombination than the other two. Diffusion lengths were determined at various places on the cells inside grains at dislocation free (white in the images) areas using line-scans with 5 µm steps (not shown). The fitted diffusion lengths were plotted versus $N_D$ in Figure 3(d). With rising doping concentration the measured diffusion length drops as well as its standard deviation (cp. error bars). The behavior of cells with varying absorber doping concentration was only determined experimentally because for a predictive theoretical simulation approach too many parameters are unknown.
Among these parameters influencing SRH lifetime are impurities (O, N, C, metals), their type, the density and structure of defects, the absorber doping itself, the ratio of impurities (O, N, C, metals), the absorber doping. Among these parameters influencing SRH lifetime are impurities (O, N, C, metals), their type, the density and structure of defects, the absorber doping itself, the ratio of impurities (O, N, C, metals), the absorber doping. Among these parameters influencing SRH lifetime are impurities (O, N, C, metals), their type, the density and structure of defects, the absorber doping itself, the ratio of impurities (O, N, C, metals), the absorber doping.

B. Thickness Variation

Illuminated J-V curves were measured in sub- and superstrate configuration for both 14 µm and 33 µm thick bifacial quasi cells with \( N_D = 2 \times 10^{16}$/cm$^3$\). The obtained mean values and standard deviations of \( J_{SC} \) and \( V_{OC} \) of all non-shunted cells were plotted as orange stars in Figure 4; the maximum values are indicated by orange lines. Note that FF and efficiency are not included because quasi cells have an inherently high base resistance so no useful information can be drawn from these values.

The devices’ \( V_{OC} \) and \( J_{SC} \) were also simulated using ASPIN3 to compare them with the measured ones. To this end, a structure representing the geometries of a quasi cell test structure was implemented into ASPIN3. The optical were adapted to real device optics measured via UV/VIS spectroscopy (not shown). The simulation domain was half the cross section in Figure 1. In the simulation, the absorber contact has to be part of the domain, but was made sufficiently small. An isolation gap of 60 µm was assumed accounting for the long cumulative ITO etching times in three consecutive acidic solutions. Mobilities of the LPC-Si with an absorber doping of \( N_D = 2 \times 10^{16}$/cm$^3$\) were set fixed to \( \mu_n = 859 \text{ cm}^2/\text{Vs} \) and \( \mu_p = 244 \text{ cm}^2/\text{Vs} \) for electrons and holes, respectively, which corresponds to 80 % of the mobilities obtained from the Masetti model [17]. The LPC-Si(n)a-Si:H(i/p) interface was assumed as non-limited and negligible in terms of its surface recombination due to the high quality passivated heterojunctions we used [25]. The parameters varied during the simulations were the effective surface recombination velocity of the LPC-Si/glass interface \( S_{eff} \) (in cm/s) and the minority bulk SRH lifetime \( \tau_p \) (in µs). To check the general validity of the approach, measured and simulated quantum efficiencies were compared (not shown). They resulted in having the same features like humps, bumps and general slope. Subsequently, J-V curves were simulated with a glass/LPC-Si interface recombination velocity of 200 cm/s and 800 cm/s. They are plotted in the first and second columns of each separate section in Figure 4, respectively. The lifetime \( \tau_p \) was varied from 0.5 µs to 20 µs in various steps. For the 800 cm/s version, only the 20 µs result is plotted. In Figure 4(a) we can see that while the current for the thin cells is equal for both illumination types, the current for the thick cells is reduced by 7 mA/cm$^2$. Yet, in substrate configuration, i.e. front emitter operation, the current is higher than for the thin cells. For a simulated \( S_{eff} \) of 200 cm/s for the thin (14 µm) cells the
behavior of a constant current independent of illumination type, can only be adequately imitated by lifetimes above 2 µs. For 800 cm/s this is not even possible with a lifetime of 20 µs. For the thick cells the simulated current shows almost no breakdown at all for 20 µs and 200 cm/s. In Figure 4(b) we can see that the overall measured VOC trend can be mimicked quite well by lifetimes of 0.5 µs – 2 µs and 200 cm/s, but the simulation fails to represent the measurement for higher lifetimes and also for a lifetime of 20 µs and 800 cm/s (partly reversed trend).

![Figure 4: Mean values and standard deviations of measured JSC (a) and VOC (b) for thin and thick cells in superstrate and substrate configurations are indicated as orange stars. The maximum values are represented by orange lines. The devices were simulated with lifetimes between 0.5 and 20 µs and glass/LPC-Si interface recombination velocities of 200 cm/s (first values in each section) and having a lifetime of 20 µs and 800 cm/s (second value in each section).](image)

III. DISCUSSION

The general trends observed for the doping concentration series are as expected from general theory. A higher ND results in lower hole mobilities μp [17] and Auger and SRH recombination begin to rise which all negatively affect the minority diffusion length Ldiff. This has a primary impact on JSC, which can be observed clearly in Figure 2. A direct proof of the decreasing diffusion lengths are also the measured values depicted in Figure 3(d) and again listed in Table I. Despite this increase in absorber recombination, the VOC rises with increasing ND, solely due to the higher absorber doping itself. This can be understood by looking at how the VOC depends on JSC, Ldiff, µp and ND. From literature it is known that the open-circuit voltage follows

\[
V_{OC} \propto V_{th} \ln \left( \frac{J_{SC}}{J_0} \right),
\]

with the thermal voltage \( V_{th} = kT/e \) (elementary charge \( e \), Boltzman constant \( k \) and absolute temperature \( T \)), the short circuit current density \( J_{SC} \), and the saturation current density \( J_0 \). The latter is a function of all other sought parameters and can be expressed as

\[
J_0 = V_{th} \cdot e \cdot n_i^2 \cdot \left( \frac{\mu_p}{L_{diff} \cdot N_D} \right),
\]

with the intrinsic carrier concentration \( n_i^2 \). Until a doping concentration of \( 1.7 \times 10^{17}/cm^3 \) VOC rises (see Figure 2). For higher ND, the losses in Ldiff (Equation 3) and JSC (Equation 2) seem to start over-compensating the impact of the doping itself and VOC sinks again slightly. However, this trend cannot be reproduced if we assume the diffusion lengths found by LBIC (Figure 3, Table I) and insert the values together with literature data for \( n_i^2 \), \( V_{th} \) and \( e \) in Eqs. (2,3) and plot them together with the measured VOC in Figure 2 (see black circles). Neither does the trend change if we take a correction factor for \( J_0 \) in Equation 2 into account; the so-called geometry factor (Jgeo) [24]. It is a correction factor for the case of a finite absorber thickness and if the emitter-sided interface is not recombination active. Hence, it can be applied for the investigated IBC-SHJ cells, since the emitter-side is a-Si:H passivated [25]. The equation for \( J_0 \) under these assumptions reads

\[
J_0 = \frac{e n_i^2 D}{N_D L_{bulk}} \left( \frac{\cosh(W_{abs} / L_{bulk})}{\sinh(W_{abs} / L_{bulk})} + D/(L_{bulk} S_{eff}) \cosh(W_{abs} / L_{bulk}) + \sinh(W_{abs} / L_{bulk}) \right),
\]

with the surface recombination velocity \( S_{eff} \) (glass/LPC-Si), the diffusion coefficient \( D \) of the minority carriers in the absorber and its thickness \( W_{abs} \). An \( S_{eff} \) of 200 cm/s was chosen for estimating Jgeo which is in accordance with results from the thickness variation on the quasi cell test structures that will be discussed later on and the using the diffusion coefficient

\[
D = V_{th} \mu_p.
\]
The bulk diffusion length $L_{\text{bulk}}$ was calculated from the effective diffusion lengths $L_{\text{diff}}$ in Table I and the assumed $S_{\text{eff}}$. We can see that the trend for the calculated $V_{\text{OC}}$ in Figure 2 including $J_{\text{fcor}}$ (black triangles) does not match the measurements. Either the assumed 80 % of the monocrystalline Si mobilities are not correct for higher $N_D$ or the effective diffusion length. Since the latter was only measured inside grains at places of high current collection (cp. white areas in Figure 3 (a-c)) and not at dislocations and grain boundaries and thus does not represent an average or global diffusion length the behavior can be explained. To make the trend match the measurement, a global diffusion length of 3-4 µm instead of the locally determined 13±1 µm would be necessary for the highest $N_D$ of 7.0·10¹⁷/cm³. The difference between measurement and calculations (Figure 2, blue and black) is much less for the lowest doping concentration, indicating that here global and locally measured diffusion length lie closer together. This can actually be explained by the 2D LBIC scans in Figure 3 (a-c) because the images at different doping concentrations show a different impact of GB/dislocations that influence the global $L_{\text{diff}}$. Note that this analytical analysis is rather crude, since we omitted the influence that a different diode ideality factor could have on the trends so the results should be regarded with care. Determining also statistics on the ideality of all the measured cells would exceed the scope of this work.

Next, it was tried to quantify the losses at GB/dislocations as already described in [11] by deriving a current collection loss percentage due to absorber inhomogeneities. Losses of 7, 11 and 15 % were measured for 2·10¹⁶, 1.7·10¹⁷ and 7·10¹⁷/cm³ absorbers, respectively, and are listed in Table I. Although this method may not be very accurate, it shows the trends quite well and furthermore the loss percentage of 11 % for $N_D = 1.7·10¹⁷$/cm³ corresponds exactly to the one obtained for a cell with a similar absorber doping investigated in [11]. We can see in the table that not only does $L_{\text{diff}}$ inside grains decrease but also the amount of losses due to GB/dislocations increases with higher doping concentration. This leads to the conclusion that a higher doping concentration can be responsible for a higher GB/dislocation density and/or greater impact of said defects in LPC-Si. The higher defect density affects $V_{\text{OC}}$, since dislocations are more difficult to passivate (both inside the absorber bulk, and in terms of the interface towards the a-Si:H), as well as $J_{\text{SC}}$ (reduced LBIC collection signal). We can see the effect on $V_{\text{OC}}$ directly when we look at the trends for measured and calculated $V_{\text{OC}}$ in Figure 2 (blue and black, respectively). If we assume the locally measured $L_{\text{diff}}$ as the overall (global) one, we get the wrong trend. The local $L_{\text{diff}}$ over-estimates the measured $V_{\text{OC}}$ more for higher $N_D$, where also the impact/losses of GB/dislocations are higher. Why the impact of defects is increased with $N_D$ is subject to speculation but might be related to the greater amount of foreign/impurity atoms (dopant atoms being counted as impurity atoms). It is known that phosphorus (P) segregates at GBs [26,27]. Mandurah et al. [27] stated that the fraction of dopant atoms segregating at GBs is inversely proportional to the size of the grains. For higher doping concentrations in LPC-Si material this would mean that (i) since more P is present, more P also segregates at the GBs, and (ii) if the grains themselves are also smaller, an even higher fraction of P segregates there creating a positive feedback. The P at the GB influences electrical conduction [27] and all kinds of other impurities precipitate there (which is used in the P diffusion gettering technique [28]).

Since all samples were co-processed and received an identical wet chemical treatment, the change in $FF$ between the samples is attributed to a difference in base doping (cp. Figure 2). This is due to lower sheet resistances leading to a lower series resistance contribution from the bulk. Between the two outer extreme doping densities, an average $FF$ difference of more than 3 % was measured. In summary, the gain in $V_{\text{OC}}$ and $FF$ towards higher doping concentrations cannot over-compensate the reduction in $J_{\text{SC}}$ so that the overall power conversion efficiency shown in Figure 2 is highest for $N_D = 2·10¹⁶$/cm³.

The observed trends from the thickness variation i.e. quasi cell test structures of 14 µm (thin) and 33 µm (thick) LPC-Si absorbers in Figure 4 allow the following conclusions. Since the measured $J_{\text{SC}}$ (orange stars) in sub- and superstrate configuration for the thin absorbers is equally high, (i) the diffusion length is sufficiently long, (ii) both front and back side are sufficiently passivated so that neither of them is limiting. The current for the thick absorbers in substrate configuration is higher, since more photons can be absorbed due to their longer path through the absorber. Their breakdown in $J_{\text{SC}}$ in superstrate configuration can be due to (i) insufficient bulk lifetime, (ii) highly recombination active glass/LPC-Si interface. The latter is unlikely to happen since both thin and thick absorber samples received the same intermediate layer (IL) between glass and LPC-Si. The only difference was the energy input of the line-source used for crystallization, which might have altered the interface quality. From a macroscopic

<table>
<thead>
<tr>
<th>Sample dopant concentration [cm⁻³]</th>
<th>2.0·10¹⁶</th>
<th>1.7·10¹⁷</th>
<th>7.0·10¹⁷</th>
</tr>
</thead>
<tbody>
<tr>
<td>Diffusion length [µm]</td>
<td>29±7</td>
<td>17±1</td>
<td>13±1</td>
</tr>
<tr>
<td>Effective lifetime [µs]</td>
<td>1.3±0.6</td>
<td>0.5±0.1</td>
<td>0.3±0.1</td>
</tr>
<tr>
<td>GB/dislocation losses [%]</td>
<td>7</td>
<td>11</td>
<td>15</td>
</tr>
<tr>
<td>average $J_{\text{SC}}$ [mA/cm²]</td>
<td>26±1</td>
<td>24±2</td>
<td>19±1</td>
</tr>
</tbody>
</table>
view on the absorber and from the general level of $V_{OC}$ and $J_{SC}$ (in substrate) we can, however, conclude that differences from the process have a negligible impact on bulk and interface quality.

To this end, we will, again, make use of $f_{geo}$ which also serves as a figure of merit to check whether bulk or interface have poorer passivation properties. The geometry factor is only determined by the two ratios (i) $W_{abs}/L_{bulk}$ and (ii) $D/(L_{bulk}S_{eff})$, and the bulk diffusion $L_{bulk}$ length being

$$L_{bulk} = \sqrt{D\tau_p} \quad ,$$

including $\tau_p$. This means $f_{geo}$ directly depends on both parameters that were varied in the simulations ($\tau_p$ and $S_{eff}$). In Figure 5 $f_{geo}$ is plotted as a function of $W_{abs}/L_{bulk}$ for several selected $D/(L_{bulk}S_{eff})$ ratios. A similar representation of this function can be found in [24]. For $L_{bulk} \geq 2W_{abs}$, the function collapses and $f_{geo}$ becomes independent of $S_{eff}$ at the LPC-Si/glass interface. For lower ratio values, two cases can be identified.

(i) for $D/(L_{bulk}S_{eff}) > 1$ the bulk has a higher recombination activity than the surface,

(ii) for $D/(L_{bulk}S_{eff}) < 1$ the LPC-Si/glass interface is limiting $J_0$ and hence increasing the absorber thickness would be beneficial for performance. For reference the $W_{abs}/L_{bulk}$ regime corresponding to a possible parameter space (1–5 $\mu$s) determined by comparing simulation and measurement in Figure 5 is added in the graph as orange hatched areas. The area for the thick absorber is shifted towards higher $W_{abs}/L_{bulk}$, where the influence of $S_{eff}$ on $f_{geo}$ and hence also on $J_0$ is smaller. If we insert also the derived $S_{eff}$ of 200 cm/s to compute $D/(L_{bulk}S_{eff})$ values for thin and thick absorbers we get values between 5 and 13, corresponding to the lower red and blue curve in the graph. The orange hatched area between these two curves is our estimate for $f_{geo}$. It tells us that the bulk material quality is limiting the performance for the investigated quasi cell test structures and thus also for the lowest doping concentration of the IBC-SHJ doping series. Consequently, it would be a futile approach to increase cell efficiency of the advanced IBC-SHJ cells (Figure 1(a)) by increasing the absorber thickness. The result of a “bulk limitation” is not sensitive to changes in both $\tau_p$ (or $L_{bulk}$) and $S_{eff}$. The ratio $D/(L_{bulk}S_{eff})$ becomes smaller than 1 (case (ii)) only if $S_{eff} \geq 1200$ cm/s assuming a bulk lifetime of 5 $\mu$s or if $S_{eff} \geq 600$ cm/s for a bulk lifetime of 20 $\mu$s. Both cases have been excluded by the previous investigation of comparing simulation with experiment in Figure 4.

![Figure 5: $f_{geo}$ as a function of $W_{abs}/L_{bulk}$ for representative values of $D/(L_{bulk}S_{eff})$. The ranges for $W_{abs}/L_{bulk}$ ratios for the absorbers of 14 $\mu$m and 33 $\mu$m are added as orange hatched areas. Lower $W_{abs}/L_{bulk}$ ratio means more influence of the front interface quality. Higher $f_{geo}$ indicates bulk limitation, lower indicates interface limitation. Note the double log-axis.](image)

Due to this, all the following conclusions drawn will be under the assumption that the material and interface quality of both thin and thick absorbers is the same and is thus also the same for the IBC-SHJ cells of the absorber doping series with the lowest $N_D$, namely 2.0 $\cdot 10^{16}$/cm$^3$. The fact that the $V_{OC}$ for the thick absorbers is slightly smaller is conforming to the fact that the $V_{OC}$ is also a function of absorber thickness. From the general picture of the $J_{SC}$ trend we can conclude that the effective diffusion length for the thin absorbers is long enough for efficient superstrate operation, while for the thick absorbers it is insufficient. This confirms the findings of the doping series (Table 1).

To compare the measurements to the simulation, we will focus more on observed trends, than on absolute values due to possible measurement errors. The trends of a breakdown in $J_{SC}$ for the thick absorber in superstrate configuration cannot be imitated correctly by a bulk lifetime of 20 $\mu$s and 200 cm/s and furthermore the simulated $V_{OC}$ are too high (Figure 4). An $S_{eff}$ of 800 cm/s fails to imitate the constant $J_{SC}$ for 14 $\mu$m in both configurations, even at 20 $\mu$s where the current saturates. Hence, $S_{eff}$ has to be smaller than 800 cm/s, and $\tau_p$ smaller than 20 $\mu$s. Furthermore, a lifetime $\tau_p = 0.5$ $\mu$s yields a too strong decrease of $J_{SC}$ from sub- to superstrate so that we can safely assume the lifetime to be greater than 0.5 $\mu$s. The corresponding $L_{diff}$ regime would be $24 \sim 43$ $\mu$m for the thin, and $25 \sim 49$ $\mu$m for the thick absorbers. This is in-line with the measurement results for the $2\cdot10^{16}$/cm$^3$ cells from the doping series (cp. Figure 3(d), Table 1). One of the objectives of the thickness variation was to find out whether LPC-Si bulk or the buried and inaccessible glass-LPC-Si interface would be limiting the performance.

<table>
<thead>
<tr>
<th>$W_{abs}/L_{bulk}$ Ratio</th>
<th>$D/(L_{bulk}S_{eff})$ Ratio</th>
<th>$f_{geo}$</th>
</tr>
</thead>
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<tr>
<td>0.0001</td>
<td>0.1</td>
<td>10</td>
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<td>10</td>
<td>1</td>
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<tr>
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<td>0.5</td>
</tr>
<tr>
<td>1</td>
<td>1000</td>
<td>0.1</td>
</tr>
<tr>
<td>2</td>
<td>10000</td>
<td>0.0001</td>
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<tr>
<td>10</td>
<td>10000</td>
<td>0.0001</td>
</tr>
</tbody>
</table>
indicates that the cell performance is much more sensitive to changes in the bulk lifetime and that increasing the bulk lifetime offers a higher potential to improve cell performance than increasing surface quality.

CONCLUSIONS

In this paper we have investigated and partly quantified the behavior of n-type liquid phase crystallized Si solar cell absorbers depending on absorber doping and absorber thickness. To this end, one IBC-SHJ cell doping series spanning almost two magnitudes of absorber doping and quasi cell test structures of two different thicknesses were fabricated. The former were analyzed via LBIC and solar simulator measurements, the latter via simulations and solar simulator measurements. We found that the inter-grain diffusion length sinks drastically with higher doping from 29±7 to 13±1 µm and that at the same time the passivation quality of grain boundaries and dislocations decreases. The latter is probably due to phosphorous segregation, which could be mitigated using gettering techniques that have so far not been tried on the multi-crystalline thin LPC-Si. The lower material quality of the higher doping leads to a break down in current that cannot be over-compensated by an increase in $V_{OC}$ and $FF$. For the highest doping concentration of $7.0 \times 10^{17}$/cm³ the $V_{OC}$ is again slightly reduced due to the impact of the grain boundaries which would yield global averaged diffusion lengths of 3-4 µm as opposed to the locally found 13 µm inside good grains.

Advanced cell concepts for LPC-Si absorbers have to be developed for superstrate (illumination through the glass) operation to make use of the inherent advantages of the LPC-Si technology. Hence, knowledge about the buried and inherently inaccessible glass/LPC-Si interface is of major importance. To get more insight into whether the LPC-Si bulk or the buried interface is limiting the performance at the current state of development, quasi cell test structures were investigated making use of their bifaciality. It was found that the intermediate layer (IL) sufficiently passivates the LPC-Si/glass interface and that, at this point, more potential to reach higher performance can be expected from improving the bulk. At the current status the bulk lifetimes are around 1-5 µs depending on local absorber quality due to the inhomogeneous multi-crystalline nature. The critical buried interface has a surface recombination velocity of around 200 cm/s. This leads to effective (overall) diffusion lengths $L_{diff}$ of 24 – 43 µm, compared to the values obtained by local LBIC investigations of (29±7 µm) for the same $N_D$ of 2.0 $\times 10^{16}$/cm³. The two values for $L_{diff}$ are in excellent agreement and thus show clearly that for low doping concentrations the GBs and dislocations in LPC-Si do not lead to a substantial breakdown of the overall $L_{diff}$. This length of $L_{diff}$ is furthermore enough to tap the full potential of ~15 µm thick absorbers. Using thicker absorbers to enhance absorption and hence $J_{SC}$ requires longer diffusion lengths that could be obtained by (i) larger grains or (ii) better passivated grains, which can be reached by gettering techniques [28], improved hydrogen passivation annealing techniques [12,14] or advanced crystallization concepts [9]. This way improving the current highest reported 13.2 % conversion efficiency [11] to above 16 % seems feasible in the future.

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